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AAROMATIC POLYCARBONATE RESIN
COMPOSITION

DECLARATION

Assistant Commissioner for Patents,
Washington, D.C.

Sir:

I, Masaharu Shizuki, declare and say:
that I am thoroughly conversant in both the Japanese and
English languages;
that I am presently engaged as translator in these
languages;

that the attached document represents a true English
translation of the Japanese Priority Application
No. 2002-319515, filed November 1, 2002.

I further declare that all statements made herein of my
own knowledge are true and that all statements made on
information and belief are believed to be true; and further
that these statements were made with the knowledge that willful
false statements and the like so made are punishable by fine
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the United States Code, and that such willful false statements
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Signed this 26th day of June, 2006.


Translator



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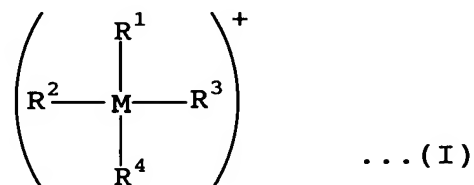
[Title of Invention] Aromatic polycarbonate resin composition

[Claims]

[Claim 1] An aromatic polycarbonate resin composition comprising:

(A) an aromatic polycarbonate (component A) and
(B) a layer silicate (component B) having 50 to 200 milliequivalents/100 g of cation exchange capacity and ion-exchanged by an organic onium ion represented by the following general formula (I), the content of the component B being 0.1 to 20 parts by weight based on 100 parts by weight of the component A.

[Formula 1]



(wherein M represents a nitrogen atom or a phosphorus atom, R^1 and R^2 represent an alkyl group having 6 to 16 carbon atoms and may be the same as or different from each other, and R^3 and R^4 represent an alkyl group having 1 to 4 carbon atoms and may be the same as or different from each other)

[Claim 2] The aromatic polycarbonate resin composition of claim 1, wherein the resin composition further comprises (C) a compound (component C) having an affinity for the aromatic polycarbonate (component A) and having a hydrophilic component being 0.1 to 50 parts by weight based on 100 parts by weight of the component A.

[Claim 3] The aromatic polycarbonate resin composition of claim 1 or 2, wherein R^1 and R^2 in the above general formula

(I), which represents an organic onium ion, relating to the component B are an alkyl group having 7 to 14 carbon atoms.

[Claim 4] The aromatic polycarbonate resin composition of claim 2 or 3, wherein the component C is a polymer having an affinity for the aromatic polycarbonate (component A) and having a functional group comprising a carboxyl group and/or a derivative thereof.

[Claim 5] The aromatic polycarbonate resin composition of claim 4, wherein the component C is a styrene-containing polymer (component C-1) having a functional group comprising a carboxyl group and/or a derivative thereof.

[Claim 6] The aromatic polycarbonate resin composition of claim 5, wherein the component C-1 is a styrene-maleic anhydride copolymer.

[Claim 7] The aromatic polycarbonate resin composition of any one of claims 2 to 6, wherein the component B and the component C are melt-kneaded in advance so as to obtain a melt-kneaded mixture with the component A.

[Claim 8] The aromatic polycarbonate resin composition of any one of claims 1 to 7, wherein the composition further comprises (D) a partial ester and/or a full ester (component D) of a higher fatty acid and a polyhydric alcohol, the component D being 0.005 to 1 part by weight based on 100 parts by weight of the component A.

[Detailed Description of the Invention]

[0001]

[Technical Field of the Invention]

The present invention relates to an aromatic polycarbonate resin composition in which a layer silicate ion-exchanged by an organic onium ion is finely dispersed. More specifically, it relates to a novel aromatic polycarbonate resin composition having high rigidity and comprising an aromatic polycarbonate in which a layer silicate ion-exchanged by an organic onium ion having a

specific molecular structure is finely dispersed, the composition having significantly improved environmental stability under a high temperature and high humidity condition, i.e., hydrolysis resistance.

[0002]

[Prior Art]

An aromatic polycarbonate having a carbonic ester bond in a recurring unit generally has excellent heat resistance, mechanical properties, impact resistance and dimensional stability and is used in a wide variety of fields of office automation equipment, automobiles, electric and electronic parts and the like. Along with a recent technological trend toward reductions in weight, thickness, length and size, the aromatic polycarbonate is required to have higher rigidity in many fields.

[0003]

As means for improving the rigidity (flexural modulus) of a thermoplastic resin, it has heretofore been generally practiced to mix a fibrous reinforcing material such as glass fibers or an inorganic filler into the thermoplastic resin. However, the conventional method has such problems that the specific gravity of a product becomes large and that the appearance of the surface of the product becomes poor.

[0004]

Meanwhile, as one of techniques for achieving a high flexural modulus by a relatively small amount of a filler, a resin composition comprising a thermoplastic resin in which a layer silicate, more preferably a layer silicate whose interlayer ions have been ion-exchanged by various organic onium ions, is finely dispersed as an inorganic filler is proposed. Further, a resin composition comprising a combination of an aromatic polycarbonate and a layer silicate whose interlayer ions have been ion-exchanged by various organic onium ions is also known (refer to Patent Publications

1 to 6).

[0005]

As the organic onium ions for ion-exchanging the interlayer ions of the layer silicate, an organic onium ion having an alkyl group having at least 12 carbon atoms as represented by a dimethyl dioctadecyl ammonium ion and an ammonium ion having a polyethylene glycol chain are proposed (refer to Patent Publications 2 and 3). Further, for all thermoplastic resins, it has been proposed that a quaternary ammonium ion having 15 to 30 carbon atoms is preferred as the organic onium ion (refer to Patent Publication 7) and that a quaternary ammonium ion (or phosphonium ion) comprising one organic group of which has at least 8 carbon atoms and other three organic groups of which have 1 to 4 carbon atoms is preferred as the organic onium ion (refer to Patent Publication 8).

[0006]

However, all these proposals suggest nothing about the hydrolysis resistance of an aromatic polycarbonate resin composition. In actuality, an aromatic polycarbonate resin composition containing a layer silicate ion-exchanged by such an organic onium ion has a problem in hydrolysis resistance. Thus, an improvement in the hydrolysis resistance of the aromatic polycarbonate resin composition containing the layer silicate is an important technical object to be achieved for the purpose of further increasing its practicality.

[0007]

[Patent Publication 1]	JP-A 3-215558
[Patent Publication 2]	JP-A 7-207134
[Patent Publication 3]	JP-A 7-228762
[Patent Publication 4]	JP-A 7-331092
(Patent Publication 5)	JP-A 9-143359
[Patent Publication 6]	JP-A 10-60160

[Patent Publication 7]

JP-A 2002-88255

[Patent Publication 8]

International

Publication Pamphlet No. WO99/32403 (Japanese Patent
laid-open publication 2001-526313)

[0008]

[Subject to Be Solved by the Invention]

Therefore, a primary object of the present invention is to provide an aromatic polycarbonate resin composition having good rigidity and good hydrolysis resistance.

[0009]

The present inventors have made intensive studies so as to achieve the above objects and found a fact that a resin composition which comprises an aromatic polycarbonate as a main component and a layer silicate ion-exchanged by a specific organic onium ion, preferably a resin composition which further comprises a compound having an affinity for the aromatic polycarbonate having a hydrophilic component, (more preferably a polymer having a functional group comprising a carboxylic group and/or a derivative thereof), further a resin composition which comprises a partial ester and/or a full ester of a higher fatty acid and polyhydric alcohol, shows significantly suppressed hydrolysis under a high temperature and high humidity condition.

Using a layer silicate ion-exchanged by a specific organic onium ion can produce a polycarbonate resin composition having a good rigidity and good hydrolysis resistance as well as a good surface appearance, even when the content of the silicate is relatively small. Then, the present inventors have made further intensive studies so as to complete the present invention on the above findings.

[0010]

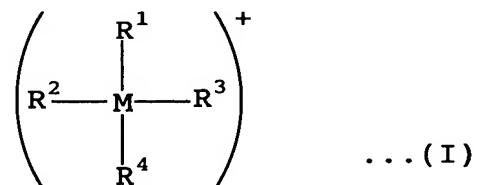
[Means for settling the subject]

The present invention relates to (1) an aromatic

polycarbonate resin composition comprising:

(A) an aromatic polycarbonate (component A) and
(B) a layer silicate (component B) having 50 to 200 milliequivalents/100 g of cation exchange capacity and ion-exchanged by an organic onium ion represented by the following general formula (I) and the content of the component B being 0.1 to 20 parts by weight (preferably, 0.5 to 15 parts by weight) based on 100 parts by weight of the component A:
[0011]

[Formula 2]



[0012]

(in the above formula (I), M represents a nitrogen atom or a phosphorus atom, R¹ and R² represent an alkyl group having 6 to 16 carbon atoms and may be the same as or different from each other, and R³ and R⁴ represent an alkyl group having 1 to 4 carbon atoms and may be the same as or different from each other.) According to the above constitution (1), there is provided an polycarbonate resin composition which has special effect (referred to as "the effect of the present invention" hereinafter), that is, having good rigidity and good hydrolysis resistance.

[0013]

A preferable embodiment of the present invention is aromatic polycarbonate resin composition of above (1), (2) comprising the composition further contains (C) a compound (component C) having an affinity for the aromatic polycarbonate (component A) and having a hydrophilic

component being 0.1 to 50 parts by weight (preferably 0.5 to 20 parts by weight) based on 100 parts by weight of the component A. there is provided an aromatic polycarbonate resin composition having effect of present invention and improved thermal stability according to the constituent (2).
[0014]

More preferable embodiment of the present invention is (3) the aromatic polycarbonate resin composition of above (1) and (2), wherein R^1 and R^2 in the above formula (I) which represents an organic onium ion, relating to the component B, are an alkyl group having 7 to 14 (preferably 7 to 12, more preferably 8 to 11) carbon atoms. There is provided an aromatic polycarbonate resin composition having remarkable effect of present invention according to the constituent (3).
[0015]

More preferable embodiment of the present invention is (4) the aromatic polycarbonate resin composition of above (2) and (3), wherein the component C is a polymer having an affinity for the aromatic polycarbonate (component A) and having a functional group comprising a carboxyl group and/or a derivative thereof. There is provided an aromatic polycarbonate resin composition having effect of present invention, and further excellent thermal stability according to the constituent (4).
[0016]

More preferable embodiment of the present invention is (5) the aromatic polycarbonate resin composition of above (4), wherein the component C is a styrene-containing polymer (component C-1) having a functional group comprising a carboxyl group and/or a derivative thereof. There is provided an aromatic polycarbonate resin composition having effect of present invention, and further excellent thermal stability according to the constituent (5).
[0017]

More preferable embodiment of the present invention is (6) the aromatic polycarbonate resin composition of above (5), wherein the component C-1 is a styrene-maleic anhydride copolymer. There is provided an aromatic polycarbonate resin composition having effect of present invention, and particularly excellent thermal stability according to the constituent (6). That is, it is the most suitable embodiment of the aromatic polycarbonate resin composition which comprises a styrene-maleic anhydride copolymer as the component C.

[0018]

More preferable embodiment of the present invention is (7) the aromatic polycarbonate resin composition of above (2) to (6), (7) wherein the component B and the component C are melt-kneaded in advance so as to obtain a melt-kneaded mixture which is then melt-kneaded with the component A. The layer silicate (component B) can be more finely dispersed to give higher rigidity and good hydrolysis resistance effectively to the resin composition according to the constituent (7). Addition to the above, the constituent (7) promotes the thermal stability of the layer silicate. There is provided an aromatic polycarbonate resin composition having more excellent effects in the present invention according to the constituent (7).

[0019]

More preferable embodiment of the present invention is (8) the aromatic polycarbonate resin composition of above (1) to (7), wherein the composition further comprises (D) a partial ester and/or a full ester (component D) of a higher fatty acid and a polyhydric alcohol, the component D being 0.005 to 1 part by weight based on 100 parts by weight of the component A. There is provided an aromatic polycarbonate resin composition having effect of present invention, and particularly excellent hydrolysis

resistance according to the constituent (8).

[0020]

[Practical Embodiment of the Invention]

Hereinafter, the components constituting the resin composition of the present invention, contents and preparation method thereof will be further described in turn.

[0021]

<About Component A>

The component A in the resin composition of the present invention is an aromatic polycarbonate which constitutes the resin composition as a main component. A representative aromatic polycarbonate is obtained by reacting a dihydric phenol with a carbonate precursor. Illustrative examples of a method of reacting the compounds include interfacial polycondensation, melt transesterification, solid-phase transesterification of a carbonate prepolymer, and ring-opening polymerization of a cyclic carbonate compound.

[0022]

Specific examples of the above dihydric phenol include hydroquinone, resorcinol, 4,4'-biphenol, 1,1-bis(4-hydroxyphenyl)ethane, 2,2-bis(4-hydroxyphenyl)propane (commonly referred to as "bisphenol A"), 2,2-bis(4-hydroxy-3-methylphenyl)propane, 2,2-bis(4-hydroxyphenyl)butane, 1,1-bis(4-hydroxyphenyl)-1-phenylethane, 1,1-bis(4-hydroxyphenyl)cyclohexane, 1,1-bis(4-hydroxyphenyl)-3,3,5-trimethylcyclohexane, 2,2-bis(4-hydroxyphenyl)pentane, 4,4'-(p-phenylenediisopropylidene)diphenol, 4,4'-(m-phenylenediisopropylidene)diphenol, 1,1-bis(4-hydroxyphenyl)-4-isopropylcyclohexane, bis(4-hydroxyphenyl)oxide, bis(4-hydroxyphenyl)sulfide, bis(4-hydroxyphenyl)sulfoxide, bis(4-hydroxyphenyl)sulfone, bis(4-hydroxyphenyl)ketone,

bis(4-hydroxyphenyl)ester,
2,2-bis(3,5-dibromo-4-hydroxyphenyl)propane,
bis(3,5-dibromo-4-hydroxyphenyl)sulfone,
bis(4-hydroxy-3-methylphenyl)sulfide,
9,9-bis(4-hydroxyphenyl)fluorene, and
9,9-bis(4-hydroxy-3-methylphenyl)fluorene. Of these, a
bis(4-hydroxyphenyl)alkane, particularly bisphenol A
(hereinafter may be abbreviated as "BPA"), is generally used.
[0023]

In the present invention, in addition to a bisphenol A based polycarbonate which is a general-purpose aromatic polycarbonate, a special aromatic polycarbonate using other dihydric phenol can be used as the component A for the purpose of attaining better hydrolysis resistance.
[0024]

For example, an aromatic polycarbonate (homopolymer or copolymer) using, as a portion or all of a dihydric phenol component, 4,4'-(m-phenylenediisopropylidene)diphenol (hereinafter may be abbreviated as "BMP"),
1,1-bis(4-hydroxyphenyl)cyclohexane,
1,1-bis(4-hydroxyphenyl-3,3,5-trimethylcyclohexane) (hereinafter may be abbreviated as "Bis-TMC"),
9,9-bis(4-hydroxyphenyl)fluorene and
9,9-bis(4-hydroxy-3-methylphenyl)fluorene (may be abbreviated as "BCF") is suitable for applications whose requirements for a dimensional change caused by water absorption and form stability are particularly stringent, because the polymer itself has good hydrolysis resistance. These dihydric phenols other than BPA are preferably used in an amount of 5 mol% or more, particularly preferably 10 mol% or more of the whole dihydric phenol component constituting the aromatic polycarbonate.
[0025]

Particularly, when high rigidity and better hydrolysis

resistance are required, the component A consisting an aromatic polycarbonate resin composition is particularly suitably any of the following copolycarbonates (1) to (3).
(1) Copolycarbonate wherein BPM constitutes 20 to 80 mol% (more suitably 40 to 75 mol%, much more suitably 45 to 65 mol%) and BCF constitutes 20 to 80 mol% (more suitably 25 to 60 mol%, much more suitably 35 to 55 mol%) out of 100 mol% of the dihydric phenol component constituting the aromatic polycarbonate.

(2) Copolycarbonate wherein BPA constitutes 10 to 95 mol% (more suitably 50 to 90 mol%, much more suitably 60 to 85 mol%) and BCF constitutes 5 to 90 mol% (more suitably 10 to 50 mol%, much more suitably 15 to 40 mol%) out of 100 mol% of the dihydric phenol component constituting the aromatic polycarbonate.

(3) Copolycarbonate wherein BPM constitutes 20 to 80 mol% (more suitably 40 to 75 mol%, much more suitably 45 to 65 mol%) and Bis-TMC constitutes 20 to 80 mol% (more suitably 25 to 60 mol%, much more suitably 35 to 55 mol%) out of 100 mol% of the dihydric phenol component constituting the aromatic polycarbonate.

[0026]

These special aromatic polycarbonates may be used alone or mixed together as appropriate before use. Further, these aromatic polycarbonates may be mixed with the generally used bisphenol A based aromatic polycarbonate and used.

[0027]

Production methods and properties of these special aromatic polycarbonates are described in detail in JP-A 6-172508, 8-27370, 2001-55435 and 2002-117580, for example.

[0028]

Of the above various aromatic polycarbonates, those having water absorption and T_g (glass transition temperature) within the following ranges by controlling

copolymerization composition or the like are particularly suitable in the field such as mirrors which must have good form stability, because the polymers themselves have good hydrolysis resistance and a significantly excellent low-warping tendency after molding.

(i) Aromatic polycarbonate having a water absorption of 0.05 to 0.15%, preferably 0.06 to 0.13%, and a Tg of 120 to 180°C.

(ii) Aromatic polycarbonate having a Tg of 160 to 250°C, preferably 170 to 230°C, and a water absorption of 0.10 to 0.30%, preferably 0.13 to 0.30%, more preferably 0.14 to 0.27%.

[0029]

The water absorption of the aromatic polycarbonate is a value of the water absorption of a disk-shaped test piece with a diameter of 45 mm and a thickness of 3.0 mm which is measured in accordance with ISO62-1980 after the piece is kept immersed in water of 23°C for 24 hours. Meanwhile, the Tg (glass transition temperature) is a value measured by a differential scanning calorimeter (DSC) in accordance with JIS K7121.

[0030]

Meanwhile, as the above carbonate precursor, a carbonyl halide, a carbonate ester or a haloformate is used. Specific examples thereof include phosgene, diphenyl carbonate, and dihaloformate of a dihydric phenol.

[0031]

In producing the polycarbonate from such a dihydric phenol and a carbonate precursor by an interfacial polymerization method, a catalyst, a terminal blocking agent and an antioxidant to prevent oxidation of the dihydric phenol may be used as required. Further, the aromatic polycarbonate may be a branched polycarbonate copolymerized with a polyfunctional aromatic compound having 3 or more functional groups. Illustrative examples of the polyfunctional

aromatic compound having 3 or more functional groups include 1,1,1-tris(4-hydroxyphenyl)ethane and 1,1,1-tris(3,5-dimethyl-4-hydroxyphenyl)ethane.

[0032]

When the polyfunctional compound producing the branched polycarbonate is contained, its amount is 0.001 to 1 mol%, preferably 0.005 to 0.9 mol%, particularly preferably 0.01 to 0.8 mol%, based on the total amount of the aromatic polycarbonate. Further, in the case of a melt transesterification method in particular, a branch structure may be produced as a side reaction. The amount of the branch structure is also 0.001 to 1 mol%, preferably 0.005 to 0.9 mol%, particularly preferably 0.01 to 0.8 mol%, based on the total amount of the aromatic polycarbonate and can be calculated by a ^1H -NMR measurement.

[0033]

Further, the aromatic polycarbonate as the component A may be a polyester carbonate copolymerized with an aromatic or aliphatic (including alicyclics) bifunctional carboxylic acid, a copolycarbonate copolymerized with a bifunctional alcohol (including alicyclics), and a polyester carbonate copolymerized with the bifunctional carboxylic acid and the bifunctional alcohol. A mixture of two or more of the obtained aromatic polycarbonates can also be used without any problem.

[0034]

As the aliphatic bifunctional carboxylic acid, α,ω -dicarboxylic acid is preferred. Preferred examples of the aliphatic bifunctional carboxylic acid include linear saturated aliphatic dicarboxylic acids such as sebacic acid (decanedioic acid), dodecanedioic acid, tetradecanedioic acid, octadecanedioic acid and icosanedioic acid; and alicyclic dicarboxylic acids such as cyclohexanedicarboxylic acid. As the bifunctional alcohol,

an alicyclic diol is more suitable. Illustrative examples of the alicyclic diol include cyclohexane dimethanol, cyclohexane diol and tricyclodecane dimethanol.

[0035]

Further, in the present invention, a polycarbonate-polyorganosiloxane copolymer copolymerized with a polyorganosiloxane unit can also be used.

[0036]

The aromatic polycarbonate which serves as the component A in the resin composition of the present invention may be a mixture of two or more of various aromatic polycarbonates including the above polycarbonates using different dihydric phenols, the above polycarbonate containing the branch component, the above polyester carbonates and the polycarbonate-polyorganosiloxane copolymer. In addition, a mixture of two or more of polycarbonates produced by different production methods and polycarbonates using different terminal blocking agents can also be used.

[0037]

The polymerization reaction of the aromatic polycarbonate by an interfacial polycondensation method is generally a reaction between a dihydric phenol and phosgene in the presence of an acid binding agent and an organic solvent. As the acid binding agent, an alkali metal hydroxide such as sodium hydroxide or potassium hydroxide or an amine compound such as pyridine is used, for example. As the organic solvent, a halogenated hydrocarbon such as methylene chloride or chlorobenzene is used, for example. Further, for the purpose of accelerating the reaction, a catalyst such as a tertiary amine, a quaternary ammonium compound or a quaternary phosphonium compound, e.g., triethylamine, tetra-n-butyl ammonium bromide and tetra-n-butyl phosphonium bromide can be used. In that case, the reaction

temperature is generally 0 to 40° C, the reaction time is about 10 minutes to 5 hours, and the pH during the reaction is preferably kept at 9 or higher.

[0038]

Further, in the polymerization reaction, a terminal blocking agent is generally used. As the terminal blocking agent, a monofunctional phenol can be used. As the monofunctional phenol, monofunctional phenols such as phenol, p-tert-butyl phenol and p-cumyl phenol are preferably used. Illustrative examples of the monofunctional phenols further include decyl phenol, dodecyl phenol, tetradecyl phenol, hexadecyl phenol, octadecyl phenol, eicosyl phenol, docosyl phenol, and triacontyl phenol. The terminal blocking agents may be used alone or in admixture of two or more.

[0039]

A reaction by a melt transesterification method is generally transesterification between a dihydric phenol and a carbonate ester. It is carried out by a method comprising mixing the dihydric phenol with the carbonate ester under heating in the presence of an inert gas and distilling out a produced alcohol or phenol. The reaction temperature ranges from 120° C to 350° C in most cases, although varying depending on the boiling point of the produced alcohol or phenol. In the late stage of the reaction, the pressure of the reaction system is reduced to about 1.33×10^3 to 13.3 Pa so as to facilitate distilling out the produced alcohol or phenol. The reaction time is about 1 to 4 hours.

[0040]

Illustrative examples of the above carbonate ester include esters of an aryl group with 6 to 10 carbon atoms which may have a substituent, an aralkyl group and an alkyl group having 1 to 4 carbon atoms. Of these, diphenyl carbonate is preferred.

[0041]

Further, a polymerization catalyst may be used to increase a polymerization rate. As the polymerization catalyst, alkali metal compounds such as sodium hydroxide, potassium hydroxide, a sodium salt of a dihydric phenol and a potassium salt of a dihydric phenol; alkaline earth metal compounds such as calcium hydroxide, barium hydroxide and magnesium hydroxide; and nitrogen-containing basic compounds such as tetramethylammonium hydroxide, tetraethylammonium hydroxide, trimethylamine and triethylamine can be used. In addition, catalysts used in an esterification reaction and a transesterification reaction such as alkoxides of alkali (earth) metals, organic acid salts of alkali (earth) metals, boron compounds, germanium compounds, antimony compounds, titanium compounds and zirconium compounds can be used. The catalysts may be used alone or in combination of two or more. These polymerization catalysts are used in an amount of preferably 1×10^{-8} to 1×10^{-3} equivalents, more preferably 1×10^{-7} to 5×10^{-4} equivalents, per mole of the dihydric phenol used as a raw material.

[0042]

In the reaction by the melt transesterification method, a compound such as 2-chlorophenylphenyl carbonate, 2-methoxycarbonylphenylphenyl carbonate or 2-ethoxycarbonylphenylphenyl carbonate can be added in the late stage of the polycondensation reaction or after completion of the polycondensation reaction so as to decrease the phenolic terminal groups of the produced polycarbonate.

[0043]

Further, in the melt transesterification method, a deactivator which neutralizes the activity of the catalyst is preferably used. The deactivator is preferably used in an amount of 0.5 to 50 moles per mole of the remaining catalyst. Further, it is preferably used in an amount of 0.01 to 500

ppm, more preferably 0.01 to 300 ppm, particularly preferably 0.01 to 100 ppm, based on the polycarbonate after polymerization. Preferred examples of the deactivator include a phosphonium salt such as tetrabutylphosphonium dodecylbenzenesulfonate and an ammonium salt such as tetraethylammonium dodecylbenzylsulfate.

[0044]

The viscosity average molecular weight of the aromatic polycarbonate which serves as the component A is not limited. However, when the viscosity average molecular weight is lower than 10,000, strength and the like deteriorate, while when it is higher than 50,000, moldability deteriorates. Thus, the viscosity average molecular weight is preferably 10,000 to 50,000, more preferably 12,000 to 30,000, much more preferably 14,000 to 28,000. In this case, a polycarbonate whose viscosity average molecular weight is out of the above range can be mixed in such an amount that moldability and the like are retained. For example, it is possible to mix a high-molecular-weight aromatic polycarbonate component having a viscosity average molecular weight of higher than 50,000.

[0045]

To calculate the viscosity average molecular weight in the present invention, a specific viscosity (η_{SP}) calculated by the following expression:

$$\text{Specific Viscosity } (\eta_{SP}) = (t - t_0)/t_0$$

(t_0 is the number of seconds taken by methylene chloride to drop, and t is the number of seconds taken by the sample solution to drop)

is firstly determined from a solution prepared by dissolving 0.7 g of aromatic polycarbonate in 100 ml of methylene chloride at 20°C by use of an Ostwald's viscometer, and a viscosity average molecular weight M is calculated from the obtained specific viscosity (η_{SP}) by the following

expression:

$$\eta_{SP}/c = [\eta] + 0.45 \times [\eta]^2 c \quad ([\eta] \text{ is a limiting viscosity})$$

$$[\eta] = 1.23 \times 10^{-4} M^{0.83}$$

$$c = 0.7$$

[0046]

The viscosity average molecular weight of the resin composition of the present invention is measured in the following manner. That is, the composition is dissolved in methylene chloride whose weight is 20 to 30 times larger than that of the composition, the soluble part is collected by filtration with celite, and the solution is then removed from the soluble part which is then fully dried so as to obtain the part soluble in methylene chloride in a solid form. A specific viscosity (η_{SP}) at 20°C is determined from a solution prepared by dissolving 0.7 g of the solid in 100 ml of methylene chloride by use of an Ostwald's viscometer, and its viscosity average molecular weight M is calculated by the above expression.

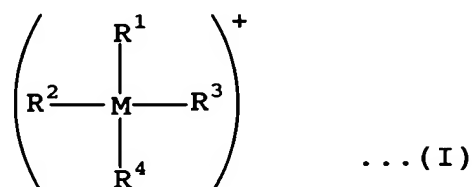
[0047]

<About Component B>

The component B which constitutes the resin composition of the present invention is a layer silicate having 50 to 200 milliequivalents/100 g of cation exchange capacity and ion-exchanged by an organic onium ion represented by the following general formula (I):

[0048]

[Formula 3]



[0049]

In the above formula (I), M represents a nitrogen atom or a phosphorus atom. Further, R^1 and R^2 each represent an

alkyl group having 6 to 16 carbon atoms and may be the same as or different from each other. R^3 and R^4 each represent an alkyl group having 1 to 4 carbon atoms and may be the same as or different from each other. In the above formula (I), R^1 and R^2 may be linear or branched. When R^3 and R^4 are a butyl group respectively, they may be linear or branched.

[0050]

These R^1 and R^2 are preferably an alkyl group having 7 to 14 carbon atoms, more preferably an alkyl group having 7 to 12 carbon atoms, much more preferably an alkyl group with 8 to 11 carbon atoms. Meanwhile, R^3 and R^4 are preferably an alkyl group having 1 to 3 carbon atoms, more preferably a methyl group or an ethyl group, much more preferably a methyl group. It is the most suitable, that is, both R^1 and R^2 are an alkyl group having 7 to 14 carbon atoms and R^3 and R^4 are a methyl group.

[0051]

Specific examples of the organic onium ion include dimethyl dioctyl ammonium, dimethyl didecyl ammonium, dimethyl didodecyl ammonium, dimethyl ditetradecyl ammonium, dimethyl dihexadecyl ammonium, diethyl didodecyl ammonium, diethyl ditetradecyl ammonium, diethyl dihexadecyl ammonium, dibutyl dioctyl ammonium, dibutyl didecyl ammonium and dibutyl didodecyl ammonium. Further, specific examples thereof also include phosphonium ions resulting from substituting nitrogen atoms in the above ammonium ions with a phosphorus atom.

[0052]

As the organic onium ion for ion-exchanging the layer silicate, a dimethyl dioctadecyl ammonium ion has conventionally been known. However, a layer silicate ion-exchanged by the organic onium ion causes poor hydrolysis resistance of the resin composition and therefore does not achieve the objects of the present invention.

[0053]

The layer silicate as the component B is a silicate or clay which comprises layers each comprising a combination of an SiO_4 tetrahedron sheet structure composed of an SiO_2 chain and an octahedron sheet structure containing Al, Mg, Li and the like, with exchangeable cations coordinated in between the layers. Representative examples of the silicate or clay include smectite-based minerals, vermiculite, halloysite and swellable micas. Specific examples of the smectite-based minerals include montmorillonite, hectorite, fluorine hectorite, saponite, beidellite and stebensite. Specific examples of the swellable micas include swellable synthetic micas such as Li-type fluorine taeniolite, Na-type fluorine taeniolite, Na-type tetrasilicon fluorine mica, and Li-type tetrasilicon fluorine mica. These layer silicates may be naturally occurring silicates or synthetic silicates. The synthetic silicates are produced by hydrothermal synthesis, melt synthesis or a solid-state reaction, for example.

[0054]

Of layer silicates, smectite-based clay minerals such as montmorillonite and hectorite and fluorine micas having swellability such as Li-type fluorine taeniolite, Na-type fluorine taeniolite and Na-type tetrasilicon fluorine mica are suitably used from the viewpoint of a cation exchange capacity and the like, and montmorillonite obtained by purifying bentonite and a synthetic fluorine mica are more suitable from the viewpoint of purity and the like. Of these, the synthetic fluorine mica which provides good mechanical properties is particularly preferred.

[0055]

The cation exchange capacity (also referred to as "cation exchange capability") of the layer silicate as the component B must be 50 to 200 milliequivalents/100 g,

preferably 80 to 150 milliequivalents/100 g, more preferably 100 to 150 milliequivalents/100 g. The cation exchange capacity is measured as a CEC value by a Schöllenger improved method which is a nationally official method as a soil standard analysis method. The cation exchange capacity of the layer silicate must be at least 50 milliequivalents/100 g so as to attain good dispersibility into the aromatic polycarbonate which is the component A. When it is larger than 200 milliequivalents/100 g, thermal degradation of the aromatic polycarbonate becomes remarkable, and an influence on thermal degradation of the aromatic polycarbonate resin composition of the present invention becomes significant. The layer silicate preferably has a pH of 7 to 10. When the value of the pH is larger than 10, the thermal stability of the aromatic polycarbonate resin composition of the present invention becomes liable to deteriorate.

[0056]

The organic onium ion in the layer silicate which is the component B is generally treated as a salt with an anion such as a halogen ion, a hydroxide ion or an acetate ion. A salt compound of the organic onium ion is reacted with a layer silicate, whereby the layer silicate as the component B is obtained.

[0057]

That is, the ion exchange of organic onium ion to layer silicate can be produced by adding an organic onium ion compound (salt compound of the organic onium ion) represented by the above formula (I) to a layer silicate dispersed in a polar solvent and collecting an ion exchanged compound to be precipitated. In general, in the ion exchange reaction, it is common to add the organic onium ion compound in an amount of 1.0 to 1.5 equivalents per equivalent of the ion exchange capacity of the layer silicate so as to exchange nearly all interlayer metal ions with the organic onium ions. However,

it is also effective for inhibiting thermal degradation of the aromatic polycarbonate to control the proportion of exchange based on the ion exchange capacity to within a given range. The proportion of ion exchange by the organic onium ion is preferably at least 40% based on the ion exchange capacity of the layer silicate. The proportion of ion exchange capacity is preferably 40 to 95 %, particularly preferably 40 to 80 %. The proportion of exchange by the organic onium ion can be calculated by determining a reduction in the weight of an exchanged compound by thermal decomposition of the organic onium ion by use of a thermogravimetry measuring device.

[0058]

<About Component C>

A suitable component C which is contained in the resin composition of the present invention is a compound having an affinity for the aromatic polycarbonate which is the component A and having a hydrophilic component. The component C produces good affinity for both the aromatic polycarbonate (component A) and the layer silicate (component B). The affinity for the two components improves the compatibilities of these two components and allows the layer silicate to be dispersed in the aromatic polycarbonate which serves as a matrix finely and stably.

[0059]

The effect of the component C with respect to dispersion of the layer silicate is assumed to be similar to that of a compatibilizer for a polymer alloy which is used for making different polymers compatible with each other. Thus, the component C is preferably a high molecular compound, i.e., a polymer, rather than a low molecular compound. Further, the polymer is more advantageous since it is excellent in thermal stability during kneading and processing. The average number of the recurring units of the polymer is

preferably 5 or more, more preferably 10 or more. Meanwhile, an upper limit on the number average molecular weight of the polymer is preferably not higher than 2,000,000. As long as the number average molecular weight does not exceed the upper limit, good moldability is obtained.

[0060]

When the component C which is contained in the resin component of the present invention is a polymer, its basic structure can be exemplified by the following examples.

a) When α is a component having an affinity for the aromatic polycarbonate and β is a hydrophilic component, a graft copolymer comprising α and β (it may be equally selected that α is a principal chain and β is a graft chain or that α is a graft chain and β is a principal chain), a block copolymer comprising α and β (the number of block segments may be 2 or more such as di- and tri-, and a radial block type and the like are included), and a random copolymer comprising α and β .

b) When α is a component having an affinity for the aromatic polycarbonate and β is a hydrophilic component, a polymer in which the function of α is expressed by the whole polymer and β is contained in α .

In the above structure a), α and β represent a polymer segment unit and a monomer unit. However, the α component is preferably the polymer segment unit from the viewpoint of an affinity for the aromatic polycarbonate. Meanwhile, the above structure b) is a case where a sufficient affinity for the aromatic polycarbonate is not expressed by α alone but a good affinity is expressed by combining α and β . There is also a case where a good affinity for the aromatic polycarbonate is expressed by α alone and the affinity is further improved by combining α with β . Thus, these structures a) and b) may partially overlap.

[0061]

As the component C in the present invention, one showing a high affinity for the aromatic polycarbonate even with the α component alone and showing a higher affinity for the polycarbonate with a combination of α and β in the whole component C is suitable.

[0062]

Next, the component (hereinafter may be referred to as " α ") having an affinity for the aromatic polycarbonate in the component C will be described in detail. As described above, since it is assumed that the component C serves in a similar manner to a compatibilizer in a polymer alloy, α is required to have a similar affinity for a polymer to that of the compatibilizer. Thus, α can be roughly classified into a non-reactive type and a reactive type.

[0063]

When the non-reactive type has the following factors, a good affinity is attained. That is, it is desired that there be, between the aromatic polycarbonate and α , factors such as (1) similarity in chemical structures, (2) closeness of solubility parameters (a difference in solubility parameter of within $1 \text{ (cal/cm}^3)^{1/2}$, i.e., within about $2.05 \text{ (MPa)}^{1/2}$ is a standard) and (3) an intermolecular interaction (such as hydrogen bonding and an interionic interaction) and a pseudo-attractive interaction peculiar to a random polymer. These factors are also known as measures for determining an affinity between a compatibilizer and a polymer which forms a base of a polymer alloy. The reactive type may be those having functional groups having reactivity with the aromatic polycarbonate in compatibilizers. Illustrative examples of the functional groups having reactivity with the aromatic polycarbonate include a carboxyl group, a carboxylic anhydride group, an epoxy group, an oxazoline group, an ester group, an ester bond, a carbonate group and a carbonate bond.

[0064]

Meanwhile, when there is a good affinity between the aromatic polycarbonate and α , there is observed a behavior that a mixture of the aromatic polycarbonate and α shows a single glass transition temperature (T_g) or a behavior that the T_g of the aromatic polycarbonate moves toward the T_g of α . Consequently, the component (α) having an affinity for the aromatic polycarbonate can be distinguished by the behaviors.

[0065]

As described above, the component (α) having an affinity for the aromatic polycarbonate in the component C is preferably a non-reactive type. In particular, it preferably exhibits a good affinity by closeness of solubility parameters. This is because the non-reactive type is superior to a reactive type in an affinity for the aromatic polycarbonate (Component A). Further, the reactive-type has a problem that thermal degradation of the polymer is promoted by a side reaction when reactivity is increased to an excessive degree.

[0066]

The solubility parameters of the aromatic polycarbonate and α in the component C preferably have the following relationship. That is, when the solubility parameter of the aromatic polycarbonate is $\delta_A((\text{MPa})^{1/2})$ and the solubility parameter of α in the component C or the solubility parameter of the whole component C is $\delta_\alpha((\text{MPa})^{1/2})$, they preferably have a relationship represented by the following formula.

$$\delta_\alpha = \delta_A \pm 2 ((\text{MPa})^{1/2})$$

[0067]

For example, since the solubility parameter of the aromatic polycarbonate which is the component A is generally about $10 (\text{cal}/\text{cm}^3)^{1/2}$ (that is, about $20.5 ((\text{MPa})^{1/2})$), δ_α is preferably 18.5 to 22.5 $((\text{MPa})^{1/2})$, more preferably 19 to

22 ((MPa)^{1/2})).

[0068]

Specific examples of a polymer component which satisfies the solubility parameter δ_a include vinyl polymers such as a styrene polymer, an alkyl(meth)acrylate polymer and an acrylonitrile polymer (as typified by, for example, a polystyrene, a styrene-maleic anhydride copolymer, a polymethyl methacrylate, a styrene-methyl methacrylate copolymer and a styrene-acrylonitrile copolymer). A polymer component having high Tg is preferably used so as to retain the heat resistance of the composition of the present invention.

[0069]

To calculate the solubility parameter, a theoretical estimation technique based on group contribution methods using the value of Small described in "Polymer Handbook - Fourth Edition" (A WILEY-INTERSCIENCE PUBLICATION, 1999) can be employed. As described above, the Tg of the aromatic polycarbonate can be measured by a differential scanning calorimeter (DSC) in accordance with JIS K7121.

[0070]

The amount of the component α having an affinity for the aromatic polycarbonate which is the component A is preferably not smaller than 5 wt%, more preferably not smaller than 10 wt%, much more preferably not smaller than 30 wt%, particularly preferably not smaller than 50 wt%, in the component C. Since the whole component C may be constituted by α , an upper limit on the amount of α can be 100 wt%.

[0071]

Meanwhile, the hydrophilic component (hereinafter may be referred to as " β ") in the component C is selected from monomers having hydrophilic groups (organic atomic groups which show a strong interaction with water) and hydrophilic polymer components (polymer segments). The hydrophilic

groups are widely known per se and exemplified by the following groups.

1) groups with strong hydrophilicity: $-\text{SO}_3\text{H}$, $-\text{SO}_3\text{M}$, $-\text{OSO}_3\text{H}$, $-\text{OSO}_3\text{M}$, $-\text{COOM}$, $-\text{NR}_3\text{X}$ (R: alkyl group, X: halogen atom, M: alkali metal, $-\text{NH}_4$) and the like.

2) groups with rather weak hydrophilicity: $-\text{COOH}$, $-\text{NH}_2$, $-\text{CN}$, $-\text{OH}$, $-\text{NHCONH}_2$ and the like.

3) groups with no hydrophilicity or weak hydrophilicity: $-\text{CH}_2\text{OCH}_3$, $-\text{OCH}_3$, $-\text{COOCH}_3$, $-\text{CS}$ and the like.

As the component C which is contained in the resin composition of the present invention, a component having a hydrophilic group classified into the above 1) or 2) is used. Above all, the hydrophilic group of the above 2) is preferred because it shows better thermal stability at the time of melt-processing of the aromatic polycarbonate. When hydrophilicity is too high, thermal degradation of the aromatic polycarbonate is liable to occur. This is because the hydrophilic group directly reacts with a carbonate bond and causes a thermal decomposition reaction.

[0072]

The hydrophilic group may be a monovalent group or a polyvalent group having at least two valences. When the component C is a polymer, a functional group with at least two valences refers to a group which does not constitute the principal chain of the polymer, and a group which constitutes the principal chain is distinguished, as a bond, from a functional group. More specifically, a group added to an atom such as carbon which constitutes the principal chain, group of a side chain and a terminal group of a molecular chain are functional groups even if they have two or more valences.

[0073]

A more specific indicator of the hydrophilic group is a solubility parameter. It is widely known that the larger

the value of the solubility parameter, the higher hydrophilicity becomes. A solubility parameter for a group can be calculated from cohesive energy (E_{coh}) for the group and a molar volume (V) for the group according to Fedors (refer to "Polymer Handbook - Fourth Edition" (A WILEY-INTERSCIENCE PUBLICATION), VII/p. 685, 1999, Polym. Eng. Sci., Vol. 14, pp. 147 and 472, 1974). Further, from the viewpoint of comparing only the degree of hydrophilicity, a numerical value (E_{coh}/V ; hereinafter "J/cm³" will be used as its unit) obtained by dividing the cohesive energy (E_{coh}) by the molar volume (V) can be used as an indicator of hydrophilicity. [0074]

The hydrophilic group contained in the hydrophilic component (β) of the component C preferably has an E_{coh}/V of 600 or larger, more preferably 800 or larger. When the E_{coh}/V is 800 or larger, it exceeds the E_{coh}/V of a carbonate bond in the aromatic polycarbonate which is the component A, indicating that the hydrophilic group has higher hydrophilicity than the carbonate bond. The E_{coh}/V is more preferably 900 or larger, much more preferably 950 or larger. Meanwhile, when hydrophilicity is too high, the thermal degradation of the aromatic polycarbonate is liable to occur as described above. Accordingly, the E_{coh}/V is preferably 2,500 or smaller, more preferably 2,000 or smaller, much more preferably 1,500 or smaller.

[0075]

As the hydrophilic component (β) in the component C, a hydrophilic polymer component (polymer segment) can also be selected. Illustrative examples of a hydrophilic polymer segment which can be β in the polymer which is the component C include a polyalkylene oxide, a polyvinyl alcohol, a polyacrylic acid, metal salts (including a chelate type) of a polyacrylic acid, a polyvinyl pyrrolidone, a polyacryl amide and a polyhydroxyethyl methacrylate. Of these, the

polyalkylene oxide, polyvinyl alcohol, polyacrylic acid, polyvinyl pyrrolidone and polyhydroxyethyl methacrylate are preferred. These are suitable since good hydrophilicity and good thermal stability for the aromatic polycarbonate (component A) (inhibition of decomposition of the aromatic polycarbonate during melt-processing) are attained simultaneously. As the polyalkylene oxide, a polyethylene oxide and a polypropylene oxide are preferred.

[0076]

In any case of the monomer having a hydrophilic group and the hydrophilic polymer component, β preferably has an acidic functional group (hereinafter may be simply referred to as "acidic group"). The acidic group inhibits thermal degradation at the time of melt-processing of the aromatic polycarbonate resin composition of the present invention. Above all, an acidic group having no nitrogen atoms is more suitable. Suitable examples of the acidic group include a carboxyl group, a carboxylic anhydride group, a sulfonic group, a sulfinic group, a phosphonic group and a phosphinic group.

[0077]

In contrast, a functional group having nitrogen atoms such as an amide group and an imide group may not inhibit the thermal degradation of the aromatic polycarbonate during melt-processing sufficiently. It is assumed that this is because the nitrogen atoms have basicity locally and cause thermal decomposition of the carbonate bond.

[0078]

When β is a monomer having a hydrophilic group, the proportion of β in the component C is 60 to 10,000, preferably 70 to 8,000, more preferably 80 to 6,000, much more preferably 100 to 3,000, in terms of a functional group equivalent which is a molecular weight per function group. Meanwhile, when β is a hydrophilic polymer segment, the proportion of β is

suitably 5 to 95 wt%, preferably 10 to 90 wt%, more preferably 30 to 70 wt%, much more preferably 30 to 50 wt%, based on 100 wt% of the component C.

[0079]

Illustrative examples of a method for producing the organic compound (component C) which comprises the component (α) having an affinity for the aromatic polycarbonate and the hydrophilic component (β) include a method comprising copolymerizing a monomer of β with a monomer constituting α , a method comprising block- or graft-copolymerizing a polymer component of β with α , and a method comprising reacting β directly with α so as to add β to α .

[0080]

Specific examples of the component C include a polymer having an affinity for the aromatic polycarbonate which is the component A and having an acidic functional group, a polymer having an affinity for the component A and having a polyalkylene oxide segment, a polymer having an affinity for the component A and having an oxazoline group, and a polymer having an affinity for the component A and having a hydroxyl group. These preferred polymers as the component C preferably have a weight average molecular weight of 10,000 to 1,000,000, more preferably 50,000 to 500,000. The weight average molecular weight is calculated as a value in terms of a polystyrene by a GPC measurement using a calibration straight line by a standard polystyrene resin.

[0081]

<About Component C-1>

Of the foregoing components C, the polymer having an affinity for the aromatic polycarbonate and having an acidic functional group is preferred, and a more preferred polymer is a polymer having an affinity for the aromatic polycarbonate and having a functional group comprising a carboxyl group and/or a derivative thereof. Further, from the viewpoint of

an effect of retaining the heat resistance of the aromatic polycarbonate, the polymer is preferably a polymer having an aromatic ring component in the principal chain and a polymer having a styrene component in the principal chain. From these viewpoints, a styrene-containing polymer (C-1 component) having a functional group comprising a carboxyl group and/or a derivative thereof is particularly suitable as the component C in the resin composition of the present invention. The styrene-containing polymer refers to a polymer containing, as a polymer component, a recurring unit resulting from polymerization of an aromatic vinyl compound such as styrene.

[0082]

The proportion of the functional group comprising a carboxyl group and/or a derivative thereof in the component C-1 is preferably 0.1 to 12 milliequivalents/g, more preferably 0.5 to 5 milliequivalents/g. 1 equivalent in the component C-1 means that 1 mole of carboxyl group exists, and its value can be calculated by back titration of potassium hydroxide or the like.

[0083]

Illustrative examples of a functional group comprising a derivative of a carboxyl group include (i) a metal salt (including a chelate salt) resulting from substituting a hydroxyl group in a carboxyl group with a metal ion, (ii) an acid chloride resulting from substituting a hydroxyl group in a carboxyl group with a chlorine atom, (iii) an ester resulting from substituting a hydroxyl group in a carboxyl group with -OR (R is a monovalent hydrocarbon group), (iv) an acid anhydride resulting from substituting a hydroxyl group in a carboxyl group with -O(CO)R (R is a monovalent hydrocarbon group), (v) an amide resulting from substituting a hydroxyl group in a carboxyl group with -NR₂ (R is hydrogen or a monovalent hydrocarbon group) and (vi) an imide resulting

from substituting hydroxyl groups in two carboxyl groups with =NR (R is hydrogen or a monovalent hydrocarbon group).

[0084]

As a method for producing the styrene-containing polymer having a functional group comprising a carboxyl group and/or a derivative thereof (hereinafter simply referred to as "carboxyl-based groups"), conventionally known methods can be used. Illustrative examples of the methods include (a) a method comprising copolymerizing a monomer having a carboxyl-based group with a styrene-based monomer and (b) a method comprising bonding or copolymerizing a compound or monomer having a carboxyl-based group with a styrene-containing polymer.

[0085]

In the above method (a), a variety of polymerization methods such as an anion living polymerization method and a group transfer polymerization method can be employed in addition to radical polymerization methods such as solution polymerization, suspension polymerization and bulk polymerization. Further, a method comprising forming a macromonomer and then carrying out polymerization can also be used. The copolymer can be used as copolymers of various forms such as an alternating copolymer, a block copolymer and a tapered copolymer in addition to a random copolymer. In the above method (b), a method can be generally employed that comprises adding a radical generator such as a peroxide or 2,3-dimethyl-2,3-diphenylbutane (generally referred to as "dicumyl") to a styrene-containing polymer or copolymer as required and reacting or copolymerizing them at high temperatures. The method thermally creates a reaction active spot in the styrene-containing polymer or copolymer and causes a compound or monomer which reacts with the active spot to react with the polymer or copolymer. Other methods of creating the active spot required for the reaction include

irradiation of radiation or an electron beam and application of an external force by a mechanochemical technique. Further, a method comprising copolymerizing a monomer which creates the active spot required for the reaction in the styrene-containing copolymer in advance can also be used. Illustrative examples of the active spot for the reaction include an unsaturated bond, a peroxide bond, and a thermally stable nitroxide radical with high steric hindrance.

[0086]

Illustrative examples of the compound or monomer having a carboxyl-based group include unsaturated monocarboxylic acids and derivatives thereof such as acrylic acid, methacrylic acid, acrylamide and methacrylamide, derivatives of maleic anhydride such as maleic anhydride, citraconic anhydride, N-phenyl maleimide and N-methyl maleimide, a glutarimide structure, and a chelate structure formed by acrylic acid and a polyvalent metal ion. Of these, a monomer having a functional group free of metal ions and a nitrogen atom is suitable, and a monomer having a carboxyl group or a carboxylic anhydride group, particularly maleic anhydride, is more suitable.

[0087]

Further, as the styrene-based monomer compound, styrene, α -methyl styrene, o-methyl styrene, m-methyl styrene, p-methyl styrene, t-butyl styrene, α -methyl vinyl toluene, dimethyl styrene, chlorostyrene, dichlorostyrene, bromostyrene, dibromostyrene and vinyl naphthalene can be used. Styrene is particularly preferred. In addition, other compounds copolymerizable with these styrene-based monomer compounds, such as acrylonitrile and methacrylonitrile, can also be used as a copolymerizable component without any problems.

[0088]

Suitable as the component C-1 in the present invention

is a styrene-containing copolymer resulting from copolymerization of a monomer having a carboxyl-based group. This is because a relatively large number of carboxyl-based groups can be contained stably in the styrene-containing polymer. A more suitable embodiment is a styrene-containing copolymer resulting from copolymerization of a monomer having a carboxyl-based group and a styrene-based monomer, and a styrene-maleic anhydride copolymer is particularly suitable. Since this styrene-maleic anhydride copolymer has high compatibility with the ion components in the layer silicate and the aromatic polycarbonate, it can finely disperse the layer silicate (B) sufficiently and can finely disperse it even to a nano order by selecting a suitable condition. Further, due to the effect of the carboxylic anhydride group, good thermal stability can be obtained in a resin composition having a layer silicate, particularly an organo-modified layered silicate. Further, since the copolymer itself has good thermal stability, it has high stability even against high-temperature conditions required for melt-processing of the aromatic polycarbonate resin.

[0089]

The composition of the styrene-containing copolymer resulting from copolymerization of a monomer having a carboxyl-based group is not limited as long as the above condition for the proportion of β is satisfied. However, a copolymer comprising 1 to 30 wt% (particularly 5 to 25 wt%) of component from a monomer having a carboxyl-based group, 99 to 70 wt% (particularly 95 to 75 wt%) of styrene-based monomer compound component and 0 to 29 wt% of other copolymerizable compound component is preferably used, and a copolymer comprising 1 to 30 wt% (particularly 5 to 25 wt%) of monomer having a carboxyl-based group and 99 to 70 wt% (particularly 95 to 75 wt%) of styrene-based monomer compound is particularly preferred.

[0090]

The molecular weight of the above component C-1 is not particularly limited. It preferably has a weight average molecular weight of 10,000 to 1,000,000, more preferably 50,000 to 500,000. The weight average molecular weight is calculated as a value in terms of a polystyrene by a GPC measurement using a calibration straight line by a standard polystyrene resin.

[0091]

<About Other Component C>

Another suitable component C is a styrene-containing copolymer (component C-2) containing an oxazoline group as a hydrophilic group. As a styrene-based monomer compound which forms the copolymer, styrene, α -methyl styrene, o-methyl styrene, m-methyl styrene, p-methyl styrene, t-butyl styrene, α -methyl vinyl toluene, dimethyl styrene, chlorostyrene, dichlorostyrene, bromostyrene, dibromostyrene and vinyl naphthalene can be used. In addition, other compounds copolymerizable with these compounds, e.g., acrylonitrile and methacrylonitrile, can also be used as a copolymerizable component without any problems. A specific example of a particularly suitable C-2 component is a styrene(2-isopropenyl-2-oxazoline)-styrene-acrylonitrile copolymer.

[0092]

Further, another suitable component C is a polyether ester copolymer (component C-3) having a polyalkylene oxide segment. The polyether ester copolymer is a polymer produced by polycondensation of a dicarboxylic acid, an alkylene glycol and a poly(alkylene oxide) glycol and their derivatives. Particularly suitable as the component C-3 is a copolymer produced from a poly(alkylene oxide)glycol having a polymerization degree of 10 to 120 or a derivative

thereof, an alkylene glycol containing at least 65 mol% of tetramethylene glycol or a derivative thereof and a dicarboxylic acid containing at least 60 mol% of terephthalic acid or a derivative thereof.

[0093]

<About Component D>

The component D which is suitably contained in the aromatic polycarbonate resin composition of the present invention is a partial ester and/or a full ester of a higher fatty acid and a polyhydric alcohol. The component D exerts an effect of further improving the hydrolysis resistance of the aromatic polycarbonate resin composition containing the layer silicate. Although the cause of the improvement in the hydrolysis resistance is unknown, it is assumed that the component D has an effect of catching an ionic compound which causes hydrolysis and neutralizing the compound.

[0094]

The higher fatty acid refers to an aliphatic carboxylic acid having 10 to 32 carbon atoms. Specific examples thereof include saturated aliphatic carboxylic acids such as decanoic acid, undecanoic acid, dodecanoic acid, tridecanoic acid, tetradecanoic acid, pentadecanoic acid, hexadecanoic acid (palmitic acid), heptadecanoic acid, octadecanoic acid (stearic acid), nonadecanoic acid, icosanoic acid, docosanoic acid and hexacosanoic acid; and unsaturated aliphatic carboxylic acids such as palmitoleic acid, oleic acid, linoleic acid, linolenic acid, eicosenoic acid, eicosapentaenoic acid and cetoleic acid. Of these, an aliphatic carboxylic acid having 10 to 22 carbon atoms is preferred, and an aliphatic carboxylic acid having 14 to 20 carbon atoms is more preferred. A saturated aliphatic carboxylic acid having 14 to 20 carbon atoms, particularly stearic acid and palmitic acid, are particularly preferred. In general, an aliphatic carboxylic acid such as stearic acid

is often a mixture containing other carboxylic acid components having different numbers of carbon atoms. In the above component D as well, an ester compound obtained from stearic acid or palmitic acid which is produced from natural oils and fats and has the form of a mixture containing other carboxylic acid components is preferably used.

[0095]

Meanwhile, the polyhydric alcohol is more preferably a polyhydric alcohol having 3 to 32 carbon atoms. Specific examples of the polyhydric alcohol include glycerine, diglycerine, a polyglycerine (such as decaglycerine), pentaerythritol, dipentaerythritol, diethylene glycol and propylene glycol.

[0096]

Of these, a partial ester of a higher fatty acid composed essentially of stearic acid and glycerine is particularly preferred as the component D. This partial ester is commercially available from, for example, Riken Vitamin Co., Ltd. with a trade name "RIKEMAL S-100A" and can be easily obtained from the market.

[0097]

<Proportions of Components>

Next, the proportions (contents) of the above components in the resin composition of the present invention will be described. The proportion of the layer silicate which is the component B is 0.1 to 20 parts by weight, preferably 0.5 to 15 parts by weight, more preferably 0.5 to 12 parts by weight, particularly preferably 1 to 10 parts by weight, based on 100 parts by weight of the component A. When the proportion of the component B is lower than the above lower limit, an effect resulting from addition of the layer silicate is not fully exhibited, so that high rigidity cannot be attained. On the other hand, when the proportion of the component B is higher than the above upper limit,

environmental stability is lowered by deterioration in the heat resistance and thermal stability of the resin composition disadvantageously.

[0098]

The effect of improving the rigidity of the resin composition is affected by the content of inorganic materials in the component B (silicate) in the resin composition. In the resin composition of the present invention, the rigidity of an article molded from the resin composition can be improved significantly even if the content of the above inorganic materials is as low as 10 wt% or less of the total. Thus, the rigidity can be improved without adverse effects on other properties due to addition of the component B. Further, an improvement in hydrolysis resistance can be achieved by use of the component B which has been ion-exchanged by a specific organic onium ion.

[0099]

Meanwhile, the component C, i.e., a compound having an affinity for the aromatic polycarbonate which is the component A and has a hydrophilic component, is preferably contained in an amount of 0.1 to 50 parts by weight based on 100 parts by weight of the component A. The proportion of the component C is more preferably 0.5 to 20 parts by weight, much more preferably 1 to 12 parts by weight, based on 100 parts by weight of the component A. Since good fine dispersion (nano dispersion) of the layer silicate and an improvement in thermal stability are achieved within the above range, an aromatic polycarbonate resin composition having higher rigidity and better thermal stability is provided. By the improvement in thermal stability, environmental stability under a high temperature and high humidity condition also becomes good.

[0100]

The proportion of the partial ester and/or full ester

of a higher fatty acid and a polyhydric alcohol as the component D is preferably 0.01 to 1 part by weight, more preferably 0.02 to 0.8 part by weight, much more preferably 0.03 to 0.5 part by weight, based on 100 parts by weight of the above component A. Within the above range, the environmental stability under a high temperature and high humidity condition is further improved. When the proportion of the component D is smaller than the above lower limit, the effect of further improving hydrolysis resistance is small, while when the proportion is larger than the above upper limit, thermal degradation of the component D itself is liable to occur disadvantageously.

[0101]

<About Additional Components can be Added as Required>

The resin composition I of the present invention is comprised of the above aromatic polycarbonate which is the component A, the layer silicate which is the component B, and the component C and D which can be suitably added. It may further contain, as additional components, polymers other than the above components and other additives as required. Illustrative examples of polymers which can be the additional components include styrene-based resins and aromatic polyester resins other than the above component C.

[0102]

As the styrene-based resins, a polystyrene (PS) (including a syndiotactic polystyrene), an impact-resistant polystyrene (HIPS), an acrylonitrile-styrene copolymer (AS resin), a methyl methacrylate-butadiene-styrene copolymer (MBS resin) and an acrylonitrile-butadiene-styrene copolymer (ABS resin) can be used. Of these, the ABS resin is the most preferable. These styrene-based resins can be used in admixture of two or more.

[0103]

As the aromatic polyester resins, a polyethylene

terephthalate (PET), a polypropylene terephthalate, a polybutylene terephthalate (PBT), a polyhexylene terephthalate, a polyethylene-2,6-naphthalate (PEN), a polybutylene naphthalate (PBN), a polyethylene-1,2-bis(phenoxy)ethane-4,4'-dicarboxylate, a polyethylene terephthalate copolymerized with 1,4-cyclohexane dimethanol (so-called PET-G), and copolyesters such as a polyethylene isophthalate/terephthalate and a polybutylene terephthalate/isophthalate can be used. Of these, the polyethylene terephthalate and the polyethylene-2,6-naphthalate are preferred. Further, when balanced moldability and mechanical properties are desired, the polybutylene terephthalate and the polybutylene naphthalate are preferred, and a blend or copolymer having a weight ratio of polybutylene terephthalate/polyethylene terephthalate of 2 to 10 is preferred. The molecular weight of the aromatic polyester resin is not particularly limited. Its intrinsic viscosity measured at 35°C using o-chlorophenol as a solvent is 0.4 to 1.2, preferably 0.6 to 1.15.

[0104]

Further, in addition to the above styrene-based resins and aromatic polyester resins, the resin composition can contain amorphous thermoplastic resins and crystalline thermoplastic resins unless they impair the object and effect of the present invention. Further, if necessary, the resin composition may also contain a flame retardant (such as a brominated epoxy resin, a brominated polystyrene, a brominated polycarbonate, a brominated polyacrylate, a monophosphate compound, a phosphate oligomer compound, a phosphonate oligomer compound, a phosphonitrile oligomer compound, a phosphonic amide compound, organic sulfonic acid alkali (earth) metal salts and a silicone-based flame

retardant), a flame retarding aid (such as sodium antimonate and antimony trioxide), an anti-dripping agent (such as a polytetrafluoroethylene capable of forming fibrils), an antioxidant (such as a hindered phenol compound and a sulfur-based antioxidant), an ultraviolet absorber, a light stabilizer, a mold releasing agent, a sliding agent, a dye, antistatic agent, a flow modifying agent, an inorganic or organic antibacterial agent, a photocatalyst-based stain-proofing agent (such as titanium oxide fine particles and zinc oxide fine particles), an infrared absorber, a photochromic agent and a fluorescent brightener.

[0105]

Preferred examples of the above dyes include a perylene-based dye, a coumarin-based dye, a thioindigo-based dye, an anthraquinone-based dye, a thioxanthone-based dye, a ferrocyanide such as Prussian blue, a perinone-based dye, a quinoline-based dye, a quinacridone-based dye, a dioxazine-based dye, an iso-indolinone-based dye and a phthalocyanine-based dye. Further, various fluorescent dyes typified by an anthraquinone-based dye, a perylene-based dye, a coumarin-based dye, a thioindigo-based dye and a thioxanthone-based dye can also be named. Further, illustrative examples of the fluorescent brightener include a bisbenzoxazolyl-stilbene derivative, a bisbenzoxazolyl-naphthalene derivative, a bisbenzoxazolyl-thiophene derivative and a coumarin-derivative.

[0106]

The aromatic polycarbonate resin composition of the present invention preferably contains a phosphorus-containing heat stabilizer. Illustrative examples of the phosphorus-containing heat stabilizer include phosphates such as trimethyl phosphate, phosphites such as triphenyl phosphite, trisnonylphenyl phosphite,

distearyl pentaerythritol diphosphite,
bis(2,6-di-t-butyl-4-methylphenyl)pentaerythritol
diphosphite, tris(2,4-di-t-butylphenyl)phosphite,
2,2-methylenebis(4,6-di-t-butylphenyl)octyl phosphite and
bis(2,4-di-t-butylphenyl)pentaerythritol diphosphite, and
phosphonites such as
tetrakis(2,4-di-t-butylphenyl)-4,4'-biphenylene
diphosphonite. The phosphorus-containing heat stabilizer
is preferably contained in an amount of 0.001 to 1 wt%, more
preferably 0.01 to 0.5 wt%, much more preferably 0.01 to 0.2
wt%, based on 100 wt% of the whole composition. By addition
of the phosphorus-containing heat stabilizer, thermal
stability is further improved and good moldability can be
obtained.

[0107]

<Preparation and Molding of the Resin Composition>

A method to prepare the aromatic polycarbonate resin composition of the present invention is optionally selected. For example, there is a method which comprises subjecting the above components and arbitrary components to premixing and then to melt kneading, pelletizing the resulting mixture thereafter. As means for the premixing, a Nauter mixer, a V-type blender, a Henschel mixer, mechanochemical equipment, an extrusion mixer and the like can be used. In the premixing, granulation can be carried out by use of an extrusion granulator, briquetting machine or the like in some cases. After the premixing, the resulting mixture is melt-kneaded by a melt-kneader typified by a vented twin-screw extruder and then pelletized by a device such as a pelletizer. In addition to the above vented twin-screw extruder, the melt-kneader may be a Banbury mixer, a kneading roll or a thermostat agitator but is preferably a multi-screw extruder typified by a vented twin-screw extruder. By use of the multi-screw extruder, the layer silicate is finely dispersed

into the component A which is a matrix resin by a more powerful shearing force.

[0108]

Further, as for the melt-kneading of the aromatic polycarbonate resin composition of the present invention by melt-kneading, a method is preferred that comprises melt-kneading the component B and the component C (suitably the component C-1) in advance and then melt-kneading the resulting product with the aromatic polycarbonate which is the component A. By the melt-kneading method, fine dispersion, preferably nano-order dispersion, of the layer silicate is achieved. Further, the melt-kneading method is preferred from a practical standpoint since it has an effect of improving the thermal stability of the aromatic polycarbonate.

[0109]

It is needless to say that the effect of the present invention is exhibited by other mixing methods. For example, there is a method which comprises mixing pellets of a resin composition comprising the components A and D with pellets obtained by melt-kneading the components B and C in advance in a molding machine (such as an injection molding machine) by feeding the pellets to the molding machine simultaneously.

[0110]

Illustrative examples of advantageous production methods of the resin composition of the present invention include (i) a method comprising melt-kneading the components B and C in a vented twin-screw extruder, pelletizing the resulting mixture and then melt-kneading the obtained pellets with the component A and (ii) a method comprising melt-kneading the components B and C in a vented twin-screw extruder by feeding them through its main feeding port and then feeding a portion or all of the component A into the melt-kneading mixture of the components B and C through a

feeding port provided in the middle portion of the twin-screw extruder. In these methods comprising melt-kneading the components B and C in advance, a portion of the component A may be involved in the melt-kneading.

[0111]

The component D can be added at any stage. For example, any of a method comprising mixing the component D with the component A in advance and then mixing the resulting mixture with other components, a method comprising adding the component D while melt-kneading the components B and C and a method comprising adding the component D in the final

[0112]

The aromatic polycarbonate resin composition of the present invention can produce a variety of products (molded articles) by injection-molding the pellets which is generally produced as above. The injection-molded articles can be obtained by using, in addition to ordinary injection molding methods, injection molding methods such as injection compression molding, injection press molding, gas assist injection molding, insert molding, in-mold coating molding, heat insulating mold molding, quick heating/cooling mold molding, two color molding, sandwich molding and ultrahigh-speed injection molding as appropriate according to purposes. The advantages of these various molding methods are already widely known. Further, as a molding system, either of a cold runner system and a hot runner system can be selected.

[0113]

Further, the aromatic polycarbonate resin composition of the present invention can also be used in the form of extrusion-molded articles of various profiles, sheets and films by extrusion molding. Further, to mold the sheets and the films, an inflation method, a calendering method or a casting method can also be used. Further, they can be molded

into a thermal shrinkable tube by a specific stretching operation. In addition, the aromatic polycarbonate resin composition of the present invention can be formed into hollow molded articles by rotational molding and blow molding.

[0114]

Further, the aromatic polycarbonate resin composition of the present invention is useful in various applications such as optical disks, various electronic and electric devices, office automation equipment, automobile parts, machine parts, agricultural materials, fishing materials, shipping containers, packaging containers and miscellaneous goods.

[0115]

The resin molded article of the present invention can be imparted with other functions by surface modification. The surface modification is means for forming a new layer on the surface of the resin molded article, e.g., deposition (such as physical vapor deposition and chemical vapor deposition), plating (such as electroplating, electroless plating and hot-dip plating), painting, coating and printing, and methods used for general resin molded articles can be employed.

[0116]

Illustrative examples of a method of laminating a metal layer or a metal oxide layer on the surface of the resin molded article include a vapor deposition method, a spraying method and a plating method. Illustrative examples of the vapor deposition method include physical vapor deposition methods such as vacuum deposition, sputtering and ion plating, and chemical vapor deposition (CVD) methods such as a thermal CVD method, a plasma CVD method and an photo-CVD method. Illustrative examples of the spraying method include an atmospheric plasma spraying method and a low-pressure plasma spraying method. Illustrative examples of the plating

method include an electroless plating (chemical plating) method, a hot-dip plating method and an electroplating method. As the electroplating method, a laser plating method can be used.

[0117]

Of the above methods, the vapor deposition method and the plating method are preferred in forming the metal layer of the resin molded article of the present invention, and the vapor deposition method is particularly preferred in forming the metal oxide layer of the resin molded article of the present invention. The vapor deposition method and the plating method may be used in combination. For example, a method comprising performing electroplating by use of a metal layer formed by the vapor deposition method can be used.

[0118]

[Example]

Hereinafter, Examples and Comparative Examples will be presented so as to describe the present invention more specifically. However, the present invention shall not be limited by them in any way. Evaluations on resin compositions were made by the following methods (1) to (4). All "parts" in the following description mean "parts by weight" unless otherwise specified.

[0119]

(1) Content of Layer Silicate (Inorganic Material)

Using a resin composition, a test piece (size: 127 mm in length \times 12.7 mm in width \times 6.4 mm in thickness) was molded by use of an injection molding machine (product of TOSHIBA MACHINE CO., LTD., trade name: IS-150EN) at a cylinder temperature of 260°C, a mold temperature of 80°C and a molding cycle of 40 seconds. The molded test piece was cut and put in a crucible so as to be weighed, heated to 600°C, kept at the temperature for 6 hours and then left to cool down, and the incineration residue remaining in the crucible was

weighed so as to measure the amount of a layer silicate (inorganic material) in the resin composition. That is, since the properties such as a flexural modulus (rigidity) of the resin composition are influenced by the proportion of the inorganic material, the proportions of inorganic materials in test pieces were measured in all Examples and Comparative Examples 2 and 3 and are shown in Table 1 as the proportion (wt%) of the inorganic material in the component B.

(2) Viscosity Average Molecular Weight, Decreasing Ratio (ΔM_{ratio}) of Viscosity Average Molecular Weight after High temperature and High Humidity Test

The viscosity average molecular weight of a test piece (size: 127 mm in length \times 12.7 mm in width \times 6.4 mm in thickness) of the same shape which was molded under the same conditions as those in the above (1) was measured by the method described in the above text. Further, the viscosity average molecular weight of the test piece (test piece after the treatment) after the test piece was left to stand in a pressure cooker at a temperature of 105°C and a relative humidity of 100% for 10 hours and then at a temperature of 23°C and a relative humidity of 50% for 24 hours and the viscosity average molecular weight of the test piece (test piece before the treatment) after the test piece was left to stand at a temperature of 23°C and a relative humidity of 50% for 74 hours were measured, and the decreasing ratio (ΔM_{ratio}) of the viscosity average molecular weight after the high temperature and high humidity test was calculated in accordance with the following expression.

$$\Delta M_{\text{ratio}} = 100 \times [(\text{viscosity average molecular weight of test piece before treatment}) - (\text{viscosity average molecular weight of test piece after treatment}) / (\text{viscosity average molecular weight of test piece before treatment})]$$

The smaller this numerical value is, the better the

hydrolysis resistance of a molded resin composition is.

(3) Surface Condition of Test Piece after High temperature and High Humidity Test

A test piece (size: 127 mm in length × 12.7 mm in width × 6.4 mm in thickness) of the same shape which was molded under the same conditions as those in the above (1) was treated under the same conditions as those in the above (2). The surface condition of the treated test piece was observed visually, and the test piece was evaluated as O when abnormalities in smoothness such as blisters and wrinkles were not observed on the surface at all and as × when abnormalities in smoothness were observed.

(4) Flexural Modulus

The flexural modulus (MPa) of a test piece (size: 127 mm in length × 12.7 mm in width × 6.4 mm in thickness) of the same shape which was molded under the same conditions as those in the above (1) was measured at a temperature of 23°C and a relative humidity of 50% in accordance with a method conforming to ASTM-D790. The larger this numerical value is, the better the rigidity of a molded resin composition is.

[0120]

(Examples 1 to 4 and Comparative Examples 1 to 3)

In one experiment (Example 4), the components shown in Table 1 were weighed and put into a polyethylene bag in the amounts shown in Table 1, and the bag was fully rotated in vertical and horizontal directions so as to dry-blend the component uniformly. This dry-blended mixture was melt-kneaded by use of a vented twin-screw extruder having a screw diameter of 30 mm [product of The Japan Steel Works, Ltd., trade name: TEX30XSST, fully intermeshing, corotating double threaded screws] so as to produce pellets. The production rate at that time was set at 20,000 g/hr, and the extrusion temperature was set at 250°C in all sections. Further, the rotation speed of the screws was set at 150 rpm,

and the degree of vacuum of the vent was set at 3 kPa. This method is shown in Table 1 as "Method 1".

[0121]

Meanwhile, in other experiments (Examples 1 to 3 and Comparative Examples 2 and 3), pellets were prepared under the same conditions as described above by a method comprising pelletizing the component B and the component C by use of the same apparatus as described above (cylinder temperature: 200°C) in advance and then mixing the pellets with other components such as the component A. This method is shown in Tables 1 to 4 as "Method 2".

[0122]

Further, in all experiments including Comparative Example 1, the following TMP (trimethyl phosphate) was added in an amount of 0.1 part by weight based on 100 parts by weight of the component A.

[0123]

The thus obtained pellets were dried by a hot air circulating dryer at 100°C for 5 hours and then formed into predetermined test pieces (size: 127 mm in length × 12.7 mm in width × 6.4 mm in thickness) by use of an injection molding machine [product of Sumitomo Heavy Industries, Ltd., trade name: SG-150U]. Molding conditions include a cylinder temperature of 260°C, a mold temperature of 80°C, a molding speed of 30 mm/sec and a pressure of around 50 MPa. The results of evaluations of these test pieces are shown in Table 1. Symbols representing the above components in Table 1 refer to the following materials.

[0124]

<Component A>

[PC-1]: bisphenol A type aromatic polycarbonate resin powder having a viscosity average molecular weight of 23,800

[product of Teijin Chemicals Ltd., "Panlite L-1250WP"]

[PC-2]: aromatic polycarbonate resin powder produced by the

following method and comprising
9,9-bis(3-methyl-4-hydroxyphenyl)fluorene (abbreviated as "BCF") and bisphenol A (abbreviated as "BPA")
[Production Method of PC-2]: 19,580 parts of ion exchange water and 3,850 parts of 48.5-wt% sodium hydroxide aqueous solution were charged into a reactor equipped with a thermometer and an agitator. In the mixture, 1,175 parts of BCF, 2,835 parts of BPA and 9 parts of hydrosulfite were dissolved, and then 13,210 parts of methylene chloride was added to the mixture. Under vigorous agitation, 2,000 parts of phosgene was blown into the resulting mixture at 15°C in about 40 minutes so as to cause a reaction. After completion of phosgene blowing, the temperature of the mixture was raised to 28°C, and 94 parts of p-t-butyl phenol and 640 parts of sodium hydroxide were added so as to cause emulsification. Then, 6 parts of triethylamine was added, and agitation was continued for 1 hour, whereby the reaction was completed. After completion of the reaction, an organic phase was separated, diluted with methylene chloride, rinsed with water, then made acidic with hydrochloric acid and rinsed with water, and when the conductivity of a water phase became nearly the same as that of the ion exchange water, methylene chloride was evaporated by a kneader, thereby obtaining 4,080 parts of colorless powder of a copolymer having a molar ratio of BCF:BPA of 20:80. The viscosity average molecular weight of this aromatic polycarbonate (PC-2) powder was 20,300.
[0125]

<Component B>

[B-1]: organo-modified synthetic fluorine mica produced by the following method and nearly completely ion-exchanged by a dimethyl di-n-decyl ammonium ion (cation exchange capacity of synthetic fluorine mica: 110 milliequivalents/100 g)
[Production Method of B-1]: About 100 parts of synthetic fluorine mica (product of Co-op Chemical Co., Ltd., "SOMASIF

ME-100") was weighed accurately and then dispersed into 10,000 parts of water (ion exchange water) of room temperature under agitation. To the dispersion, a chloride of the above onium ion (dimethyl di-n-decyl ammonium chloride) was added in an amount of 1.2 times as many equivalents as the cation exchange equivalent of the synthetic fluorine mica, and the mixture was agitated for 6 hours. The produced solid precipitate was separated by filtration, then washed in 30,000 parts of ion exchange water by agitation and then separated by filtration again. The washing and the filtration were carried out three times, respectively. The obtained solid was air-dried for 5 days, then ground in a mortar, then dried by hot air at 50° C for 10 hours, and ground in a mortar again until a maximum particle diameter of about 100 μ m was obtained. A residual water content evaluated by a reduction in thermogravimetry when kept under a flow of nitrogen at 120° C for 1 hour by the hot air drying was 3 wt%. Thereby, B-1 was obtained.

[B-2]: organo-modified synthetic fluorine mica produced by the following method and having 55% of cation exchange capacity thereof ion-exchanged by a dimethyl di-n-decyl ammonium ion (cation exchange capacity of synthetic fluorine mica: 110 milliequivalents/100 g)

[Production Method of B-2]: B-2 was produced in the same manner as in the case of the above B-1 except that dimethyl di-n-decyl ammonium chloride was added in an amount of 0.8 times as many equivalents as the cation exchange equivalent of the synthetic fluorine mica in the production method of the above B-1.

[0126]

<Layer Silicates out of Scope of Present Invention>

For comparison, the following B-3 and B-4 were used as layer silicates ion-exchanged by organic onium ions which were out of the scope of the present invention.

[B-3]: organo-modified synthetic fluorine mica nearly completely ion-exchanged by tri-n-octyl methyl ammonium chloride (product of Co-op Chemical Co., Ltd., "SOMASIF MTE", cation exchange capacity of synthetic fluorine mica: 110 milliequivalents/100 g)

[B-4]: organo-modified synthetic fluorine mica nearly completely ion-exchanged by dimethyl di-n-octadecyl ammonium chloride (product of Co-op Chemical Co., Ltd., "SOMASIF MAE", cation exchange capacity of synthetic fluorine mica: 110 milliequivalents/100 g)

[0127]

<Component C>

[C-1]: styrene-maleic anhydride copolymer (product of Nova Chemicals Japan Ltd., "DYLARK 332-80", amount of maleic anhydride: about 15 wt%)

[C-2]: (2-isopropenyl-2-oxazoline)-styrene-acrylonitrile copolymer (product of Nippon Shokubai Co., Ltd., "EPOCROS RAS-1005", amount of 2-isopropenyl-2-oxazoline: about 5 wt%)

<Component D>

[D-1]: partial or full ester of a higher fatty acid and a polyhydric alcohol (product of Riken Vitamin Co., Ltd., "RIKEMAL S-100A")

(Other Components)

TMP: trimethyl phosphate (product of DAIHACHI CHEMICAL INDUSTRY CO., LTD., trade name: TMP), added in an amount of 0.1 parts by weight based on 100 parts by weight of the component A in every case.

[0128]

[Table 1]

Composition	Component	Symbol	Unit	Ex.1	Ex.2	Ex.3	Ex.4
	Component A	PC-1	Parts by Weight	100	100	100	-
Composition	Component B or Similar Component Thereof	PC-2	Parts by Weight	-	-	-	100
		B-1	Parts by Weight	4.2		8.5	4.2
		B-2	Parts by Weight	-	3.9	-	-
		B-3	Parts by Weight	-	-	-	-
	Component C	B-4	Parts by Weight	-	-	-	-
		C-1	Parts by Weight	6	6	12	-
		C-2	Parts by Weight	-	-	-	6
	Component D	D-1	Parts by Weight	-	0.3	0.3	0.3
Properties	Proportion of Inorganic Material in Component B in Composition			2.5	2.4	5.1	2.4
	Production Method		-	Method 2	Method 2	Method 2	Method 1
	Viscosity Average Molecular Weight		-	21,300	22,100	20,200	15,800
	ΔM ratio		%	14.1	9.8	12.4	14.6
	Surface Appearance		Visual Evaluation	○	○	○	○
	Flexural Modulus		MPa	3,090	3,020	3,790	3,290

Ex.: Example

Table 1

Composition	Component	Symbol	Unit	C.Ex.1	C.Ex.2	C.Ex.3
	Component A	PC-1	Parts by Weight	100	100	100
Component B or Similar Thereof		PC-2	Parts by Weight	-	-	-
		B-1	Parts by Weight	-	-	-
		B-2	Parts by Weight	-	-	-
		B-3	Parts by Weight	-	8.7	-
Component C		B-4	Parts by Weight	-	-	4.6
		C-1	Parts by Weight	-	12	6
		C-2	Parts by Weight	-	-	-
Component D		D-1	Parts by Weight	-	-	0.3
	Proportion of Inorganic Material in Component B in Composition		% by Weight	-	5	2.4
	Production Method		-	-	Method 2	Method 2
Properties	Viscosity Average Molecular Weight		-	23,800	19,700	17,700
	ΔM ratio		%	6.1	36.0	33.9
	Surface Appearance		Visual Evaluation	○	×	×
	Flexural Modulus		MPa	2,110	3,880	3,140

C.Ex.: Comparative Example

[0129]

As is obvious from the results shown in Table 1, the aromatic polycarbonate resin compositions (Examples 1 to 4) containing the layer silicates (B-1 and B-2) ion-exchanged by the organic onium ions specified in the present invention undergo only a small decrease in molecular weight when exposed to a high temperature and high humidity environment and show excellent hydrolysis resistance and a high flexural modulus (rigidity), and molded articles thereof have good surface appearances. In contrast, it is obvious that the ordinary aromatic polycarbonate resin (Comparative Example 1) containing no layer silicate has poor rigidity and that the resin compositions (Comparative Examples 2 and 3) containing the layer silicates (B-3 and B-4) ion-exchanged by the organic onium ions different from those specified in the present invention have improved rigidity, but the molecular weights had decreased when the resin composition was produced and molded articles thereof show poor hydrolysis resistance when exposed to a high temperature and high humidity environment and also have poor surface appearances.

[0130]

[Effect of the Invention]

As above, the aromatic polycarbonate resin composition of the present invention have high rigidity which has not heretofore been achieved and have hydrolysis resistance. Further, the resin composition also has such advantages that it has good moldability and give a molded article having a good surface appearance, particularly good surface smoothness. These properties give higher practical use of the aromatic polycarbonate resin composition, which is useful in a wide variety of applications such as various electronic and electric devices, office automation equipment, automobile parts, machine parts, agricultural materials, fishing materials, shipping containers, packaging

containers and miscellaneous goods. The compositions are extremely valuable from an industrial standpoint.

[Title of Document] Abstract

[Abstract]

[Subject] To provide an aromatic polycarbonate resin composition having good rigidity and good hydrolysis resistance.

[Means of Solution]

 An aromatic polycarbonate resin composition comprising:

(A) 100 parts by weight of aromatic polycarbonate (component A)

(B) 0.1 to 20 parts by weight of layer silicate (component B) having 50 to 200 milliequivalents/100 g of cation exchange capacity and ion-exchanged by an organic onium ion which is a n alkyl sulfonium ion having a specific structure, further

(C) 0.1 to 50 parts by weight of compound (component C) having an affinity for the component A and having a hydrophilic component, and

(D) 0.005 to 1 part by weight of partial and/or full ester (component D) of a higher fatty acid and a polyhydric alcohol.

[Selected Drawing] nil